

Transient growth in Poiseuille-Rayleigh-Bénard flows of binary fluids with Soret effect*

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Abstract The transient growth due to non-normality is investigated for the Poiseuille-Rayleigh-Bénard problem of binary fluids with the Soret effect. For negative separation factors such as $\psi = -0.1$, it is found that a large transient growth can be obtained by the non-normal interaction of the two least-stable-modes, i.e., the upstream and downstream modes, which determine the linear critical boundary curves for small Reynolds numbers. The transient growth is so strong that the optimal energy amplification factor $G(t)$ is up to $10^2 \sim 10^3$. While for positive separation factors such as $\psi = 0.1$, the transient growth is weak with the order $O(1)$ of the amplification factor, which can even be computed by the least-stable-mode. However, for both cases, the least-stable-mode can govern the long-term behavior of the amplification factor for large time. The results also show that large Reynolds numbers have stabilization effects for the maximum amplification within moderate wave number regions. Meanwhile, much small negative or large positive separation factors and large Rayleigh numbers can enlarge the maximum transient growth of the pure streamwise disturbance with the wavenumber $\alpha = 3.14$. Moreover, the initial and evolutionary two-dimensional spatial patterns of the large transient growth for the pure streamwise disturbance are exhibited with a plot of the velocity vector, spanwise vorticity, temperature, and concentration field. The initial three-layer cell vorticity structure is revealed. When the amplification factor reaches the maximum G_{\max} , it develops into one cell structure with large amplification for the vorticity strength.

Key words binary fluid, Soret effect, transient growth, Poiseuille-Rayleigh-Bénard flow

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1 Introduction

The mixed convection in binary mixtures with the Soret effect has many practical applications, e.g., chemical vapour deposition (CVD) in the electronic industry. It also leads to rich and complex spatiotemporal pattern formations, which have a great theoretical interest. In fact, the already rich spatiotemporal behavior of the dissipative structures occurring in binary mixture convection^[1] may be affected by the externally imposed through-flow. It is why the Poiseuille-Rayleigh-Bénard flows have been intensively studied for small Reynolds numbers^[2–5] by linear, nonlinear, and transient behaviors, dealing with either temporal or spatiotemporal instabilities.

How a horizontal plane Poiseuille shear flow changes the linear convection properties in heated binary fluid layers was first investigated by Jung et al.^[2]. They solved the full linear stability equations by a shooting method for realistic top and bottom boundary conditions, and found that the through-flow broke the symmetrical left and right traveling waves (TW), and the frequencies, bifurcation thresholds, and structural properties of the two symmetry degenerate TW solution branches as well as the stationary overturning convection (SOC) were changed dramatically. Later, Büchel and Lücke^[3] studied the effect of a horizontal through-flow with small Reynolds numbers on stationary and traveling wave convective patterns with a Galerkin expansion and a finite difference numerical method. The bifurcation diagrams of various quantities, e.g., the Nusselt number, the frequency, and the mixing behavior, are determined as functions of the heating rate and the wave number for several through-flow rates and the Soret coupling strengths for the ethanol-water parameters. They also studied the growth dynamics of small convective perturbations into different and strongly nonlinear convective states and the transition between them.

Concerning the study of the absolute and convective instability, the boundary curves separating these two types of instabilities for both negative separation factors (corresponding to the two symmetry degenerate TW solutions) and positive separation factors (corresponding to the SOC solution) were first plotted as a function of the through-flow rate by Jung et al.^[2]. Later, Büchel and Lücke^[4] studied the spatiotemporal properties of the spatially localized convective perturbations in detail for heated binary fluid layers with or without a through-flow. The fronts and pulse-like wave packets formed out of the three relevant perturbations (two oscillatory perturbations and a stationary perturbation) were analyzed after evaluating the appropriate saddle points of the three respective dispersion relations of the linear stability equations over the complex wave number plane. Jung and Lücke^[5] further compared the spatiotemporal properties of the fronts obtained from the saddle point analysis of the dispersion relation of the linear field equations with the numerical solutions of the full nonlinear hydrodynamical equations. Using the Chebyshev collocation method to solve the full linear stability equations, Hu et al.^[6] investigated the temporal and spatiotemporal instabilities of the Poiseuille-Rayleigh-Bénard flows for much larger Reynolds numbers. For positive separation factors, they found that the critical thresholds strongly increased when the through-flow was used, and the boundary curves between the absolute instability (AI) and the convective instability (CI) increased as well, but more steeply. For enough large positive separation factors, there existed three local minima in the neutral curves $Ra(k)$ (the Rayleigh number against the wavenumber) for moderate Reynolds numbers, resulting in the discontinuity of the critical wavenumber curve and the non-smoothness of the critical Rayleigh number curve when the Reynolds number varied. For negative separation factors, there existed a contact point between the critical Rayleigh number curve and the AI/CI boundary curve, at which the fluid system directly changed from stable to absolutely unstable without crossing the convectively unstable region. Through an energy budget analysis for the binary fluid system, it was found that, when the separation was positive (negative), the solutal buoyancy contribution would make the system unstable (stable).

It is well-known that the effect of the non-normality in plane Poiseuille, Couette, or other

channel flows can enable large transient growth prior to eventual exponential decay^[7–11]. For optimal disturbances for plane Poiseuille flows, the Orr-mechanism and lift-up mechanism have been revealed to be responsible for the two-dimensional and three-dimensional optimal disturbances, respectively. For optimal disturbances for the Poiseuille-Rayleigh-Bénard flows of pure fluids, it has also been found^[12] that streamwise-uniform perturbations can produce large streamwise streaks and Rayleigh-Bénard convection rolls at moderately large Reynolds numbers for all Rayleigh numbers and Prandtl numbers. The transient growth of linearly stable disturbances is believed to play an important role in the subcritical transition of many flow systems, especially for shear flows. It has already been revealed that the Poiseuille-Rayleigh-Bénard flows are subcritically unstable for negative separation factors^[3], while their non-normal transient growth has not been intensively studied. This constitutes the main content of this paper.

2 Formulation

We consider a non-reactive binary fluid mixture contained in an infinite horizontal channel of the height H (see Fig. 1). The binary mixture is heated as follows. The horizontal boundaries are isothermal and held at different temperatures. The temperature at the top wall ($z = H$) is T_2 , the temperature at the bottom wall ($z = 0$) is T_1 , and $T_1 > T_2$. A through-flow in the x -direction is also driven by imposing a constant pressure gradient along the channel. The resulting global flow is usually called the Poiseuille-Rayleigh-Bénard flow. Due to the gravitational effect, the binary mixture may become unstable when the vertical temperature and concentration gradients exist. To take this into account, the Boussinesq approximation is used such that the density variations are restricted to the buoyancy term, and are expressed as a linear law, i.e.,

$$\rho = \rho_0(1 - \beta_T(T - T_0) - \beta_C(C - C_0)), \tag{1}$$

where β_T and β_C are the thermal and solutal expansion coefficients, respectively, ρ_0 , T_0 , and C_0 are the reference values for the density, temperature, and concentration, respectively, which are taken as mean values.

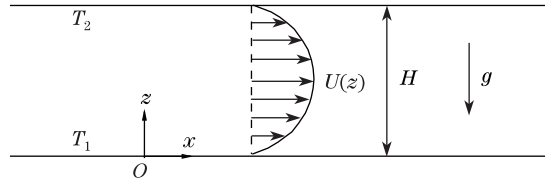


Fig. 1 Schematic representation of Poiseuille-Rayleigh-Bénard model

The Soret effect, which arises as the contribution of the increase in the temperature gradient to the mass flux, is considered here, whereas the Dufour effect, which arises as the contribution of the increase in the concentration gradient to the heat flux, is neglected. The mass flux J_C and the heat flux J_T are

$$J_C = -\rho_0 D_C \nabla C - \rho_0 D_S \nabla T, \quad J_T = -D_T \nabla T, \tag{2}$$

where D_C , D_S , and D_T are the solutal diffusion coefficient, the Soret diffusion coefficient, and the thermal conductivity, respectively. The conductive steady state will then correspond to the linear variations along the z -direction for both the temperature and the concentration, leading to a concentration difference

$$\Delta C = -\frac{D_S \Delta T}{D_C},$$

where $\Delta T = T_1 - T_2$.

The flow in this system is modelled by the Navier-Stokes equations coupled to an energy equation and a concentration equation. In these equations, the length, velocity, time, and pressure are scaled by H , κ/H , H^2/κ , and $\rho_0\kappa^2/H^2$, respectively, where κ is the thermal diffusivity. The dimensionless temperature θ and concentration c are, respectively, defined by

$$\frac{T - T_0}{\Delta T} \quad \text{and} \quad \frac{C - C_0}{\Delta C}.$$

Thus, the dimensionless governing equations of the three-dimensional Poiseuille-Rayleigh-Bénard flow are

$$\nabla \cdot \mathbf{v} = 0, \tag{3a}$$

$$\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} = -\nabla p + Pr \nabla^2 \mathbf{v} + Ra Pr (\theta + \psi c) \mathbf{e}_z, \tag{3b}$$

$$\frac{\partial \theta}{\partial t} + \mathbf{v} \cdot \nabla \theta = \nabla^2 \theta, \tag{3c}$$

$$\frac{\partial c}{\partial t} + \mathbf{v} \cdot \nabla c = Le (\nabla^2 c - \nabla^2 \theta), \tag{3d}$$

where $\mathbf{v} = (u, v, w)$ is the three-dimensional dimensionless velocity vector, \mathbf{e}_z is the unit vector in the vertical direction, and the operators are

$$\nabla = (\partial_x, \partial_y, \partial_z), \quad \nabla^2 = \partial_x^2 + \partial_y^2 + \partial_z^2.$$

The dimensionless parameters appearing in Eq. (3) are the Prandtl number Pr , the Rayleigh number Ra , the separation factor ψ , and the Lewis number Le defined by

$$\begin{cases} Pr = \frac{\nu}{\kappa}, & Ra = \frac{\beta_T g H^3}{\kappa \nu} \Delta T, \\ \psi = -\frac{\beta_C D_S}{\beta_T D_C}, & Le = \frac{D_c}{\kappa}, \end{cases}$$

where ν is the kinematic viscosity. The corresponding boundary conditions are

$$\text{no-slip conditions: } u = v = w = 0 \quad \text{at } z = 0, 1, \tag{4a}$$

$$\text{thermal conditions: } \theta = 0.5 \quad \text{at } z = 0, \tag{4b}$$

$$\theta = -0.5 \quad \text{at } z = 1, \tag{4c}$$

$$\text{mass impermeability: } \partial_z \theta - \partial_z c = 0 \quad \text{at } z = 0, 1. \tag{4d}$$

The non-dimensional basic steady state can easily be obtained, and corresponds to a parabolic z -profile for the x -component of the velocity vector (throughflow), a constant pressure gradient responsible for this throughflow, and a vertical pressure gradient to balance the vertical density variations and to linearize the conductive z -profiles for the temperature and concentration, i.e.,

$$\bar{u}(z) = -6RePr(z^2 - z), \tag{5a}$$

$$\nabla \bar{p} = -12RePr^2 \mathbf{e}_x + RaPr(1 + \psi)(0.5 - z) \mathbf{e}_z, \tag{5b}$$

$$\bar{\theta}(z) = 0.5 - z, \tag{5c}$$

$$\bar{c}(z) = 0.5 - z, \tag{5d}$$

where $Re = U_0 H / \nu$ is the Reynolds number, and U_0 is the dimensional mean velocity obtained by integration over the channel height.

The disturbed three-dimensional Poiseuille-Rayleigh-Bénard flow with the Soret effect can be decomposed as follows:

$$\begin{cases} u = \bar{u} + u', & v = v', & w = w', \\ p = \bar{p} + p', & \theta = \bar{\theta} + \theta', & c = \bar{c} + c'. \end{cases}$$

Then, the perturbations u' , v' , w' , p' , θ' , and c' are the solutions of the following equations:

$$\nabla \cdot \mathbf{v}' = 0, \quad (6a)$$

$$\frac{\partial u'}{\partial t} + \mathbf{v}' \cdot \nabla u' + \bar{u} \frac{\partial u'}{\partial x} + \frac{d\bar{u}}{dz} w' = -\frac{\partial p'}{\partial x} + Pr \nabla^2 u', \quad (6b)$$

$$\frac{\partial v'}{\partial t} + \mathbf{v}' \cdot \nabla v' + \bar{u} \frac{\partial v'}{\partial x} = -\frac{\partial p'}{\partial y} + Pr \nabla^2 v', \quad (6c)$$

$$\frac{\partial w'}{\partial t} + \mathbf{v}' \cdot \nabla w' + \bar{u} \frac{\partial w'}{\partial x} = -\frac{\partial p'}{\partial z} + Pr \nabla^2 w' + Ra Pr (\theta' + \psi c'), \quad (6d)$$

$$\frac{\partial \theta'}{\partial t} + \mathbf{v}' \cdot \nabla \theta' + \bar{u} \frac{\partial \theta'}{\partial x} + \frac{d\bar{\theta}}{dz} w' = \nabla^2 \theta', \quad (6e)$$

$$\frac{\partial c'}{\partial t} + \mathbf{v}' \cdot \nabla c' + \bar{u} \frac{\partial c'}{\partial x} + \frac{d\bar{c}}{dz} w' = Le (\nabla^2 c' - \nabla^2 \theta'), \quad (6f)$$

where $\mathbf{v}' = (u', v', w')$. Furthermore, by neglecting the quadratic term with respect to small disturbance, we can obtain the following linearized perturbation equations:

$$\nabla \cdot \mathbf{v}' = 0, \quad (7a)$$

$$\frac{\partial u'}{\partial t} + \bar{u} \frac{\partial u'}{\partial x} + \frac{d\bar{u}}{dz} w' = -\frac{\partial p'}{\partial x} + Pr \nabla^2 u', \quad (7b)$$

$$\frac{\partial v'}{\partial t} + \bar{u} \frac{\partial v'}{\partial x} = -\frac{\partial p'}{\partial y} + Pr \nabla^2 v', \quad (7c)$$

$$\frac{\partial w'}{\partial t} + \bar{u} \frac{\partial w'}{\partial x} = -\frac{\partial p'}{\partial z} + Pr \nabla^2 w' + Ra Pr (\theta' + \psi c'), \quad (7d)$$

$$\frac{\partial \theta'}{\partial t} + \bar{u} \frac{\partial \theta'}{\partial x} + \frac{d\bar{\theta}}{dz} w' = \nabla^2 \theta', \quad (7e)$$

$$\frac{\partial c'}{\partial t} + \bar{u} \frac{\partial c'}{\partial x} + \frac{d\bar{c}}{dz} w' = Le (\nabla^2 c' - \nabla^2 \theta'). \quad (7f)$$

The corresponding boundary conditions are

$$\text{no-slip conditions: } u' = v' = w' = 0 \quad \text{at } z = 0, 1, \quad (8a)$$

$$\text{thermal conditions: } \theta' = 0 \quad \text{at } z = 0, 1, \quad (8b)$$

$$\text{mass impermeability: } \partial_z \theta' - \partial_z c' = 0 \quad \text{at } z = 0, 1. \quad (8c)$$

Taking the divergence of the linearized momentum equations (7b), (7c), and (7d) and using Eq. (7a) yield an equation for the pressure perturbation as follows:

$$\nabla^2 p' = -2 \frac{d\bar{u}}{dz} \frac{\partial w'}{\partial x} + Ra Pr \left(\frac{\partial \theta'}{\partial z} + \psi \frac{\partial c'}{\partial z} \right). \quad (9)$$

This equation may be used with Eq. (7d) to eliminate p' , resulting in an equation for the normal velocity as follows:

$$\begin{aligned} & \left(\left(\frac{\partial}{\partial t} + \bar{u} \frac{\partial}{\partial x} \right) \nabla^2 - \frac{d^2 \bar{u}}{dz^2} \frac{\partial}{\partial x} - Pr \nabla^4 \right) w' \\ &= Ra Pr \left(\nabla_{\perp}^2 \theta' + \psi \nabla_{\perp}^2 c' \right), \end{aligned} \quad (10)$$

where

$$\nabla_{\perp}^2 = \partial_x^2 + \partial_y^2.$$

To describe the complete three-dimensional flow field, an additional equation is needed. The most convenient way is to write the equation for the vorticity perturbation along z , i.e.,

$$\zeta' = \frac{\partial u'}{\partial y} - \frac{\partial v'}{\partial x}.$$

Then, we can obtain

$$\left(\frac{\partial}{\partial t} + \bar{u} \frac{\partial}{\partial x} - Pr \nabla^2 \right) \zeta' = - \frac{d\bar{u}}{dz} \frac{\partial w'}{\partial y}. \quad (11)$$

Thus, the linearized perturbation equations can be written as follows:

$$\left(\left(\frac{\partial}{\partial t} + \bar{u} \frac{\partial}{\partial x} \right) \nabla^2 - \frac{d^2 \bar{u}}{dz^2} \frac{\partial}{\partial x} - Pr \nabla^4 \right) w' = Ra Pr \left(\nabla_{\perp}^2 \theta' + \psi \nabla_{\perp}^2 c' \right), \quad (12a)$$

$$\left(\frac{\partial}{\partial t} + \bar{u} \frac{\partial}{\partial x} - Pr \nabla^2 \right) \zeta' = - \frac{d\bar{u}}{dz} \frac{\partial w'}{\partial y}, \quad (12b)$$

$$\frac{\partial \theta'}{\partial t} + \bar{u} \frac{\partial \theta'}{\partial x} + \frac{d\bar{\theta}}{dz} w' = \nabla^2 \theta', \quad (12c)$$

$$\frac{\partial c'}{\partial t} + \bar{u} \frac{\partial c'}{\partial x} + \frac{d\bar{c}}{dz} w' = Le (\nabla^2 c' - \nabla^2 \theta'). \quad (12d)$$

These equations associated with the boundary conditions

$$\text{no-slip conditions: } w' = \frac{\partial w'}{\partial z} = \zeta' = 0 \quad \text{at } z = 0, 1, \quad (13a)$$

$$\text{thermal conditions: } \theta' = 0 \quad \text{at } z = 0, 1, \quad (13b)$$

$$\text{mass impermeability: } \partial_z \theta' - \partial_z c' = 0 \quad \text{at } z = 0, 1 \quad (13c)$$

and the initial conditions

$$w'(x, y, z, t = 0) = w'_0(x, y, z), \quad (14a)$$

$$\zeta'(x, y, z, t = 0) = \zeta'_0(x, y, z), \quad (14b)$$

$$\theta'(x, y, z, t = 0) = \theta'_0(x, y, z), \quad (14c)$$

$$c'(x, y, z, t = 0) = c'_0(x, y, z) \quad (14d)$$

provide a complete description for the evolution of an arbitrary small disturbance in both space and time.

The perturbation quantities can further be expanded as exponential functions of time and the following streamwise and spanwise coordinates:

$$(u', v', w', \zeta', p', \theta', c') = (\hat{u}(z), \hat{v}(z), \hat{w}(z), \hat{\zeta}(z), \hat{p}(z), \hat{\theta}(z), \hat{c}(z))e^{i(\alpha x + \beta y - \omega t)}. \tag{15}$$

From Eqs. (12a)–(13c), we can see that $\hat{w}(z)$, $\hat{\zeta}(z)$, $\hat{\theta}(z)$, and $\hat{c}(z)$ are independent eigenfunctions, from which the other functions $\hat{u}(z)$, $\hat{v}(z)$ and $\hat{p}(z)$ can be recovered easily as follows:

$$\hat{u} = \frac{i}{k^2}(\alpha \mathcal{D}\hat{w} - \beta \hat{\zeta}), \tag{16a}$$

$$\hat{v} = \frac{i}{k^2}(\beta \mathcal{D}\hat{w} + \alpha \hat{\zeta}), \tag{16b}$$

$$(\mathcal{D}^2 - k^2)\hat{p} = -2i\alpha \mathcal{D}\bar{u}\hat{w} + Ra \cdot Pr(\mathcal{D}\hat{\theta} + \psi \mathcal{D}\hat{c}), \tag{16c}$$

where

$$\mathcal{D} = d/dz, \quad k^2 = \alpha^2 + \beta^2.$$

After substituting Eq. (15) into Eqs. (12a)–(13c), the independent eigenfunctions can be obtained by solving the following eigenvalue problem:

$$((-i\omega + i\alpha\bar{u})(\mathcal{D}^2 - k^2) - i\alpha \mathcal{D}^2\bar{u} - Pr(\mathcal{D}^2 - k^2)^2)\hat{w} + Ra Pr k^2(\hat{\theta} + \psi \hat{c}) = 0, \tag{17a}$$

$$((-i\omega + i\alpha\bar{u}) - Pr(\mathcal{D}^2 - k^2))\hat{\zeta} + i\beta \mathcal{D}\bar{u}\hat{w} = 0, \tag{17b}$$

$$((-i\omega + i\alpha\bar{u}) - (\mathcal{D}^2 - k^2))\hat{\theta} + \mathcal{D}\bar{\theta}\hat{w} = 0, \tag{17c}$$

$$((-i\omega + i\alpha\bar{u}) - Le(\mathcal{D}^2 - k^2))\hat{c} + Le(\mathcal{D}^2 - k^2)\hat{\theta} + \mathcal{D}\bar{c}\hat{w} = 0. \tag{17d}$$

Introduce

$$\hat{\mathbf{q}} = (\hat{w}, \hat{\zeta}, \hat{\theta}, \hat{\eta})^T, \quad \hat{\eta} = \hat{\theta} - \hat{c}.$$

Then, the above linear stability equations can be rewritten as follows:

$$-i\omega \mathbf{M}\hat{\mathbf{q}} = \mathbf{L}\hat{\mathbf{q}} \tag{18}$$

with the boundary conditions

$$\hat{w} = \mathcal{D}\hat{w} = \hat{\zeta} = \hat{\theta} = \mathcal{D}\hat{\eta} = 0 \quad \text{at} \quad z = 0, 1. \tag{19}$$

The expressions of the matrices are

$$\mathbf{M} = \begin{pmatrix} k^2 - \mathcal{D}^2 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & -1 & 1 \end{pmatrix}, \tag{20}$$

$$\mathbf{L} = \begin{pmatrix} \mathcal{L}_{OS} & 0 & RaPr(1 + \psi)k^2 & -RaPr\psi k^2 \\ -i\beta\mathcal{D}\bar{u} & \mathcal{L}_{SQ} & 0 & 0 \\ -\mathcal{D}\bar{\theta} & 0 & \mathcal{L}_{TH} & 0 \\ \mathcal{D}\bar{c} & 0 & i\alpha\bar{u} & \mathcal{L}_{CO} \end{pmatrix}, \tag{21}$$

$$\mathcal{L}_{OS} = -i\alpha\bar{u}(k^2 - \mathcal{D}^2) - i\alpha\mathcal{D}^2\bar{u} - Pr(k^2 - \mathcal{D}^2)^2, \tag{22}$$

$$\mathcal{L}_{SQ} = -i\alpha\bar{u} - Pr(k^2 - \mathcal{D}^2), \tag{23}$$

$$\mathcal{L}_{TH} = -i\alpha\bar{u} - (k^2 - \mathcal{D}^2), \tag{24}$$

$$\mathcal{L}_{CO} = -i\alpha\bar{u} - Le(k^2 - \mathcal{D}^2). \tag{25}$$

Equation (17a)–(17d) are ordinary differential equations in terms of $\widehat{w}(z)$, $\widehat{\zeta}(z)$, $\widehat{\theta}(z)$, and $\widehat{\eta}(z)$, and can be regarded as a two-point boundary value problem. If there exists a nontrivial solution for the equations, a corresponding dispersion relation

$$D(\alpha, \beta, \omega; Ra, Re, \psi, Pr, Le) = 0 \tag{26}$$

should be satisfied. We need to solve an eigenvalue problem. Because it is impossible to find the explicit analytical dispersion relation if there is no further simplification, the dispersion relation has to be obtained numerically. A shooting method has been adopted for this problem in the paper of Jung et al.^[2] In this paper, the pseudospectral Chebyshev method^[13] is used to discretize the eigenvalue problem, and the QZ algorithm is used to solve the resulting general eigenvalue problem.

In order to study the transient growth of the Poiseuille-Rayleigh-Bénard flows for binary fluids, we need to derive a physically meaningful way to measure the size of the perturbation. Thus, we define a modified kinetic energy of the perturbation by

$$\begin{aligned} E(t) &= \frac{1}{2} \int_0^1 (|\widehat{u}|^2 + |\widehat{v}|^2 + |\widehat{w}|^2 + (|\widehat{\theta}|^2 + |\widehat{c}|^2)/k^2) dz \\ &= \frac{1}{2k^2} \int_0^1 (|\mathcal{D}\widehat{w}|^2 + k^2|\widehat{w}|^2 + |\widehat{\zeta}|^2 + |\widehat{\theta}|^2 + |\widehat{c}|^2) dz \\ &= \frac{1}{2k^2} \int_0^1 \begin{pmatrix} \widehat{w} \\ \widehat{\zeta} \\ \widehat{\theta} \\ \widehat{c} \end{pmatrix}^H \begin{pmatrix} k^2 - \mathcal{D}^2 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \widehat{w} \\ \widehat{\zeta} \\ \widehat{\theta} \\ \widehat{c} \end{pmatrix} dz \\ &= \frac{1}{2k^2} \int_0^1 \begin{pmatrix} \widehat{w} \\ \widehat{\zeta} \\ \widehat{\theta} \\ \widehat{\eta} \end{pmatrix}^H \begin{pmatrix} k^2 - \mathcal{D}^2 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 2 & -1 \\ 0 & 0 & -1 & 1 \end{pmatrix} \begin{pmatrix} \widehat{w} \\ \widehat{\zeta} \\ \widehat{\theta} \\ \widehat{\eta} \end{pmatrix} dz, \end{aligned} \tag{27}$$

where the superscript H indicates the conjugate transpose. The involved matrix is a positive defined weight matrix, so that a norm and inner product can be defined by

$$\|\widehat{\mathbf{q}}\|^2 = \langle \widehat{\mathbf{q}}, \widehat{\mathbf{q}} \rangle = E(t). \tag{28}$$

The initial linearized problem (12) can also be written as follows:

$$\frac{\partial}{\partial t} \widetilde{\mathbf{q}} = \mathbf{L}_1 \widetilde{\mathbf{q}}, \tag{29}$$

where

$$\begin{cases} \mathbf{L}_1 = \mathbf{M}^{-1}\mathbf{L}, & \tilde{\mathbf{q}} = (w', \zeta', \theta', \eta')^T, \\ \tilde{\mathbf{q}}(t=0) = \tilde{\mathbf{q}}_0, & \eta' = \theta' - c'. \end{cases}$$

The solution $\tilde{\mathbf{q}}$ can be expressed as follows:

$$\tilde{\mathbf{q}} = \sum_{n=1}^{\infty} \kappa_n^0 \hat{\mathbf{q}}_n e^{\lambda_n t} = \sum_{n=1}^{\infty} \kappa_n(t) \hat{\mathbf{q}}_n, \quad (30)$$

where $\hat{\mathbf{q}}_n$ is the eigenvector of the eigen-system (17) associated with the eigenvalue $\lambda_n = -i\omega_n$. Following the same methodology used in the monograph of Schmid and Henningson^[11], we project the exact solution onto the subspace S^N spanned by the eigenvectors of the N least-stable eigenvalues $(\lambda_1, \lambda_2, \dots, \lambda_N)$ of the spectrum of \mathbf{L}_1 , i.e.,

$$S^N = \text{span} \{ \hat{\mathbf{q}}_1, \hat{\mathbf{q}}_2, \dots, \hat{\mathbf{q}}_N \}.$$

The approximated solution $\tilde{\tilde{\mathbf{q}}}$ is obtained from the truncation of the exact series solution (30). Then, we can write

$$\tilde{\mathbf{q}} \approx \tilde{\tilde{\mathbf{q}}} = \sum_{n=1}^N \kappa_n^0 \hat{\mathbf{q}}_n e^{\lambda_n t} = \sum_{n=1}^N \kappa_n(t) \hat{\mathbf{q}}_n, \quad \tilde{\tilde{\mathbf{q}}} \in S^N. \quad (31)$$

If we define

$$\boldsymbol{\kappa} = \begin{pmatrix} \kappa_1 \\ \kappa_2 \\ \vdots \\ \kappa_N \end{pmatrix} = \begin{pmatrix} e^{\lambda_1 t} & & & \\ & e^{\lambda_2 t} & & \\ & & \ddots & \\ & & & e^{\lambda_N t} \end{pmatrix} \begin{pmatrix} \kappa_1^0 \\ \kappa_2^0 \\ \vdots \\ \kappa_N^0 \end{pmatrix} = e^{\Lambda t} \boldsymbol{\kappa}^0, \quad \mathbf{Q} = (\hat{\mathbf{q}}_1, \hat{\mathbf{q}}_2, \dots, \hat{\mathbf{q}}_N), \quad (32)$$

then

$$\tilde{\tilde{\mathbf{q}}} = \mathbf{Q}\boldsymbol{\kappa}, \quad (33)$$

and

$$\langle \tilde{\tilde{\mathbf{q}}}, \tilde{\tilde{\mathbf{q}}} \rangle = \sum_{m=1}^N \sum_{n=1}^N \kappa_m \kappa_n^* \langle \hat{\mathbf{q}}_n, \hat{\mathbf{q}}_m \rangle = \boldsymbol{\kappa}^H \mathbf{A} \boldsymbol{\kappa}, \quad (34)$$

where \mathbf{A} , in which $A_{nm} = \langle \hat{\mathbf{q}}_n, \hat{\mathbf{q}}_m \rangle$, is a Hermitian matrix, which can be decomposed as $\mathbf{A} = \mathbf{F}^H \mathbf{F}$ (the Cholesky decomposition). Therefore, we can obtain

$$\langle \tilde{\tilde{\mathbf{q}}}, \tilde{\tilde{\mathbf{q}}} \rangle = \boldsymbol{\kappa}^H \mathbf{F}^H \mathbf{F} \boldsymbol{\kappa} = \|\mathbf{F}\boldsymbol{\kappa}\|_2^2, \quad (35)$$

where $\|\cdot\|_2$ is the L_2 -norm (sum of squares). From Eq. (28), we can approximate the energy of the perturbation as follows:

$$E(t) \approx \|\mathbf{F}\boldsymbol{\kappa}\|_2^2 = \|\boldsymbol{\kappa}\|_{\mathbb{E}}^2. \quad (36)$$

We want to estimate the growth of a perturbation initially given by $\boldsymbol{\kappa}^0$ as a function of time. We define the energy amplification factor $g(t)$ as the ratio between the energy of the perturbation at the time t and its initial energy, i.e.,

$$g(t) = \frac{E(t)}{E(0)} \approx \frac{\|\mathbf{F}\boldsymbol{\kappa}(t)\|_2^2}{\|\mathbf{F}\boldsymbol{\kappa}^0\|_2^2} = \frac{\|\boldsymbol{\kappa}(t)\|_{\mathbb{E}}^2}{\|\boldsymbol{\kappa}^0\|_{\mathbb{E}}^2}. \quad (37)$$

For a fixed time t , we want to maximize $g(t)$ over the set of all possible initial conditions κ^0 . This maximization leads to the optimal energy amplification factor $G(t)$ as follows:

$$G(t) = \max_{E(0) \neq 0} \frac{E(t)}{E(0)} \approx \max_{\kappa^0 \neq 0} \frac{\|\mathbf{F}\kappa\|_2^2}{\|\mathbf{F}\kappa^0\|_2^2} = \max_{\kappa^0 \neq 0} \frac{\|\mathbf{F}e^{\Lambda t}\kappa^0\|_2^2}{\|\mathbf{F}\kappa^0\|_2^2} = \|\mathbf{F}e^{\Lambda t}\mathbf{F}^{-1}\|_2^2. \quad (38)$$

The quantity $G(t)$ gives the maximum amplification optimized over all possible initial conditions. In general, each point on the curve $G(t)$ is arrived at by an independent initial condition, and $G(t)$ represents the envelope of the individual growth curves. For the computation of $G(t)$, the key step is to use a singular value decomposition of the matrix \mathbf{A} to obtain the matrix \mathbf{F} , and then a singular value decomposition of the matrix $\mathbf{F}e^{\Lambda t}\mathbf{F}^{-1}$ is performed at each chosen time t . The concrete arithmetic for the plane Poiseuille flow can be found in Ref. [11].

3 Numerical results

We first consider the transient growth for the negative separation factor $\psi = -0.1$ and the small Reynolds number $Re = 0.15$ (see Fig. 2), which shows the optimal energy amplification factor $G(t)$ for the optimal disturbances to the linearly stable and unstable Poiseuille-Rayleigh-Bénard flows with the stream-wise wave number $\alpha = 3.14$ and $\beta = 0$.

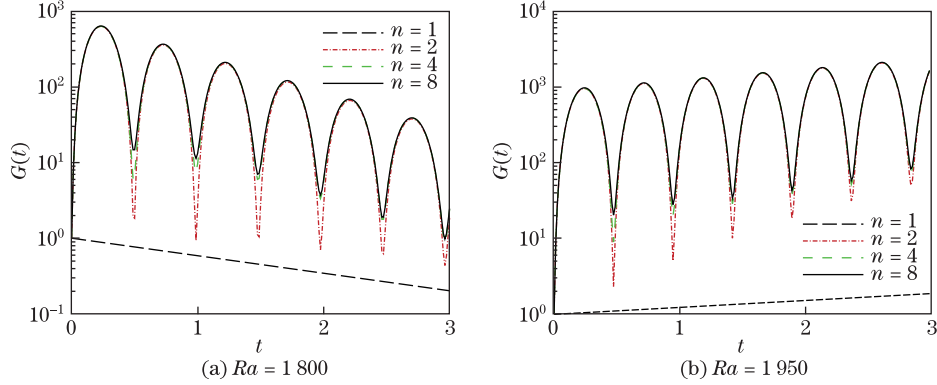


Fig. 2 Optimal energy amplification factor $G(t)$ as function of time t for Poiseuille-Rayleigh-Bénard flows of binary fluids with Soret effect and $Ra = 1800$ (linearly stable), 1950 (linearly unstable), where $\alpha = 3.14$, $\beta = 0.0$, $\psi = -0.1$, $Re = 0.15$, $Pr = 10$, and $Le = 0.01$

From Fig. 2, we can see that the initial transient growth can achieve a large amplification with the order $10^2 \sim 10^3$. The maximum amplification occurring at $t \approx 0.233$ can be obtained only by the two least-stable modes ($N = 2$), i.e., the upstream and downstream modes, and it has little change when the number of the least-stable modes increases from $N = 2$ to $N = 4, 8$. After the initial transient growth, a global cycle appears with a period T , and finally exponentially damps or amplifies for the linearly stable or unstable flow due to the dominated effect of the least-stable mode. Interestingly, it is found that the cycle period is connected to the angular frequency difference of the upstream and downstream modes with $T \approx 2\pi/|\omega_{1r} - \omega_{2r}|$. For $Ra = 1800$, the angular frequencies of the upstream and downstream modes are $\omega_{1r} = -0.10294646$, and $\omega_{2r} = 12.61900485$, and the period T is about 0.494 , agreeing with Fig. 2(a). While for $Ra = 1950$, the angular frequencies are $\omega_{1r} = -0.35549672$, and $\omega_{2r} = 12.85576413$, and the period T is about 0.4756 , agreeing with Fig. 2(b). It is thus verified that the global periodic cycle of the optimal energy amplification is only determined by the non-normal interaction of the upstream and downstream modes. The addition of the least-stable modes affects the optimal growth only slightly for long time.

For the positive separation factor $\psi = 0.1$ with the same Reynolds number and stream-wise wave number, we plot Fig.3 to present the optimal energy amplification factor $G(t)$ for the optimal disturbances to the linearly stable and unstable flows. It is easily found that the initial transient growth achieves only when the maximum amplification of the order $O(1)$ is near $t = 1$, which is far smaller than that for the negative separation factor $\psi = -0.1$. In addition, it is clearly seen that the least-stable mode will govern the exponential behavior of the optimal growth function for long time ($t > 2$) without the existence of the periodic cycle like $\psi = -0.1$. Furthermore, with the increase in the number in the least-stable modes to plot the optimal energy amplification, the characteristics of the transient growth change significantly, and obviously, the optimal energy amplification for $N = 14$ is nearly three times larger than that for $N = 9$.

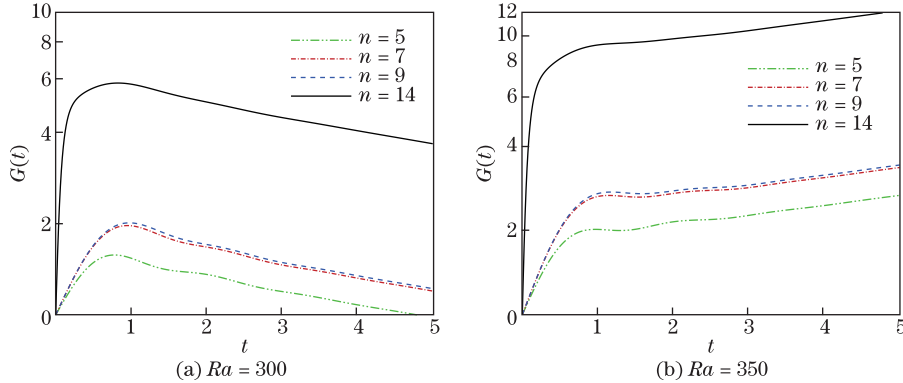


Fig. 3 Optimal energy amplification factor $G(t)$ as function of time t for Poiseuille-Rayleigh-Bénard flows of binary fluids with Soret effect and $Ra = 300$ (linearly stable), 350 (linearly unstable), where $\alpha = 3.14$, $\beta = 0.0$, $\psi = 0.1$, $Re = 0.15$, $Pr = 10$, and $Le = 0.01$

Let us now further examine the maximum growth function $G_{\max} = \max_t G(t)$ in the $\alpha\beta$ -plane for Poiseuille-Rayleigh-Bénard flows of binary fluids with the Soret effect (see Fig. 4). It is found that, for the negative separation factor $\psi = -0.1$ and the Rayleigh number $Ra = 1800$ shown in Fig. 4(a), the distributions of the maximum growth function are like concentric circles, while the optimum of G_{\max} is about 885. This growth is achieved for $\alpha = 0.0$ and $\beta \approx 4.0$. In addition, we find that it occurs at the time $t \approx 0.174$. For the positive separation factor $\psi = 0.1$ and the Rayleigh number $Ra = 300$ shown in Fig. 4(b), it is found that due to the

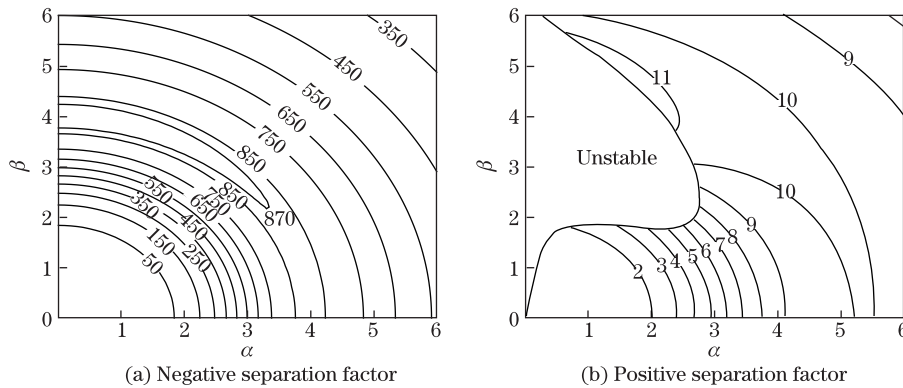


Fig. 4 Contours of maximum transient growth G_{\max} in $\alpha\beta$ -plane for Poiseuille-Rayleigh-Bénard flows of binary fluids with Soret effect and negative separation factor ($\psi = -0.1$, $Ra = 1800$) or positive separation factor ($\psi = 0.1$, $Ra = 300$), where $Re = 0.15$, $Pr = 10$, and $Le = 0.01$ ($N = 31$ least-stable spectra are used)

squire transformation for the least-stable OS mode, there exists a large unstable eigenvalue region in the $\alpha\beta$ -plane, where $G_{\max} = \infty$ for $t \rightarrow \infty$. It is bounded by the bold solid neutral curve shown in Fig. 4(b). The optimum of G_{\max} is near the contour line $G_{\max} = 11$, and exactly occurs at the neutral curve. For the pure stream-wise disturbance, it is found that the optimum of G_{\max} is located at $\alpha \approx 5.4$.

3.1 Reynolds number dependence of optimal transient growth

So far, only a small Reynolds number $Re = 0.15$ has been investigated for the optimal transient growth of the Poiseuille-Rayleigh-Bénard flows. It is necessary to study the Reynolds number dependence of the optimal transient growth with pure streamwise disturbance for the negative separation factor $\psi = -0.1$ ($Ra = 1800$) and positive separation factor $\psi = 0.1$ ($Ra = 300$) (see Fig. 5). Figure 5(a) shows that, for the stream-wise disturbances with long or moderate wavelength ($\alpha < 3$), the Reynolds number effect on the optimal transient growth is very weak, while for large stream-wise wave numbers ($\alpha > 3$), with the increase in the Reynolds number, the maximum growth function decreases, showing that the inertial effect has a stabilized effect on the transient growth. Furthermore, it is clearly seen that the stabilizing role of the inertia is the most significant for the wavenumber $\alpha \approx 4.0$. Thus, the optimum of G_{\max} occurs at $Re = 0$ and $\alpha \approx 4.0$. In Fig. 5(b), there exists an unstable region for small Reynolds numbers, beyond which the characteristics of the transient growth are similar to those in Fig. 5(a), i.e., with the increase in the Reynolds number, the maximum growth function decreases. This stabilization effect also occurs at much larger wave number region.

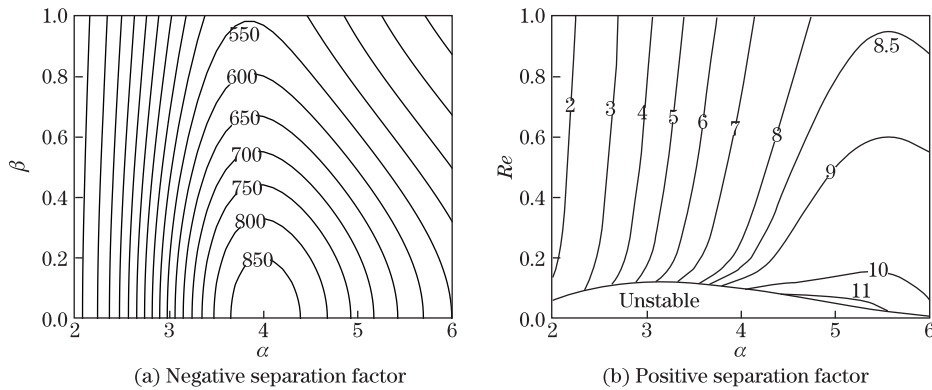


Fig. 5 Contours of maximum transient growth G_{\max} in αRe -plane for Poiseuille-Rayleigh-Bénard flows of binary fluids with Soret effect and negative separation factor ($\psi = -0.1$, $Ra = 1800$) or positive separation factor ($\psi = 0.1$, $Ra = 300$), where $\beta = 0.0$, $Pr = 10$, and $Le = 0.01$ ($N = 31$ least-stable spectra are used)

3.2 Separation factor and Rayleigh number dependence

As mentioned above, for the stream-wise disturbance with $\alpha = 3.14$, the variation of small Reynolds numbers has a slight effect on the maximum transient growth. Therefore, under this situation, it is convenient to study the combined effects of the separation factor and Rayleigh number on the optimal transient growth with the small Reynolds number $Re = 0.15$. For this purpose, the contours of the maximum transient growth G_{\max} are plotted in Fig. 6 for both negative and positive separation factors. Figure 6(a) shows an unstable region on the upper right corner, beyond which the maximum growth function increases to the order $O(10^3)$ with the increase in the Rayleigh number and the decrease in the separation factor. This reveals an important fact that small negative separation factors can make very large transient amplification though the flow system needs a large Rayleigh number to become linearly unstable. From Fig. 6(b), it is found that the contour curve of the maximum transient growth is parallel to the ψ - Ra neutral curve, and the increases in the Rayleigh number and the positive separation factor can produce larger transient amplification with the order $O(1)$.

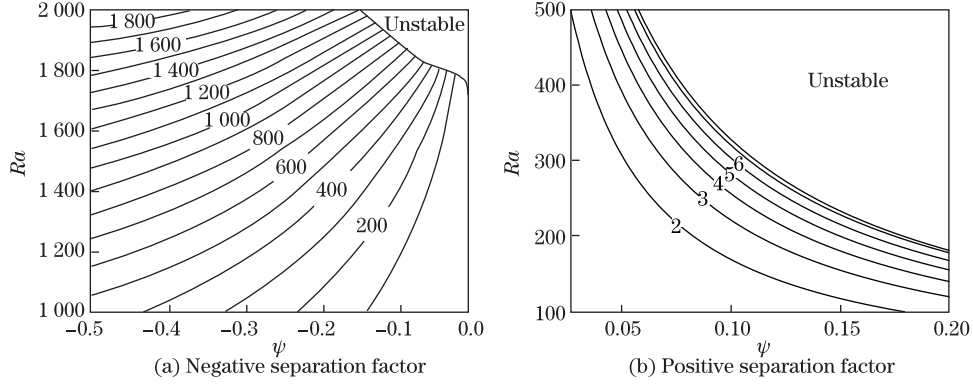


Fig. 6 Contours of maximum transient growth G_{\max} in ψRa -plane for Poiseuille-Rayleigh-Bénard flows of binary fluids with Soret effect and negative or positive separation factor, where $\alpha = 3.14$, $\beta = 0.0$, $Re = 0.15$, $Pr = 10$, and $Le = 0.01$ ($N = 31$ least-stable spectra are used)

3.3 Spatial pattern of optimal disturbances for large transient growth

Similar to our usual understanding of the perturbation pattern at the critical points of the flow instability onset, it is also instructive and interesting to exhibit the pattern of the initial disturbance that gives the largest amplification for a given time. From the definition (38) of the optimal energy amplification factor, a singular value decomposition (SVD) should be performed, i.e.,

$$\mathbf{F}e^{\Lambda t}\mathbf{F}^{-1} = \mathbf{U}\Sigma\mathbf{V}^H \rightarrow \mathbf{F}e^{\Lambda t}\mathbf{F}^{-1}\mathbf{V} = \mathbf{U}\Sigma. \quad (39)$$

Obviously, the largest singular value is just the square root of $G(t)$, and the the singular vectors in \mathbf{V} and \mathbf{U} associated with the largest singular value are, respectively, the desired optimal initial condition and the maximum amplified spatial pattern at a given time. Usually, the singular values are ordered in a decreasing manner. Therefore, the first columns of \mathbf{V} and \mathbf{U} are our desired singular vectors, and we denote them as \mathbf{V}_1 and \mathbf{U}_1 , respectively. Then, the optimal initial condition can be obtained from

$$\tilde{\mathbf{q}}_0 = \sum_{n=1}^N \kappa_n^0 \hat{\mathbf{q}}_n = \mathbf{Q}\kappa^0 = \mathbf{Q}\mathbf{F}^{-1}\mathbf{V}_1, \quad (40)$$

and the spatial pattern at the given time t_{spec} evolved from the above initial optimal disturbance can be obtained by

$$\tilde{\mathbf{q}}_{\text{opt}} = \sum_{n=1}^N \kappa_n^{\text{opt}} \hat{\mathbf{q}}_n = \mathbf{Q}\kappa(t_{\text{spec}}) = \mathbf{Q}e^{\Lambda t_{\text{spec}}}\mathbf{F}^{-1}\mathbf{V}_1 = \sigma_1\mathbf{Q}\mathbf{F}^{-1}\mathbf{U}_1, \quad (41)$$

where σ_1 is the largest (principal) singular value.

As we have already known, a large transient growth can be obtained by the two-dimensional pure optimal stream-wise disturbance for the negative separation factor $\psi = -0.1$ (see Fig. 2(a)). The maximum optimal amplification occurs at $t_{\text{max}} \approx 0.233$. Thus, we can perform the singular value decomposition of $\mathbf{F}e^{\Lambda t_{\text{max}}}\mathbf{F}^{-1}$ to get \mathbf{V}_1 and \mathbf{U}_1 for this maximum optimal amplification. Then, from Eqs.(40) and (41), we can obtain the optimal initial and evolutionary spatial patterns, whose velocity vector (u, w) , spanwise vorticity ξ , temperature θ , and concentration c fields are plotted in Fig. 7.

It is easily seen from Fig. 7(a) that the initial velocity field of the optimal disturbance has

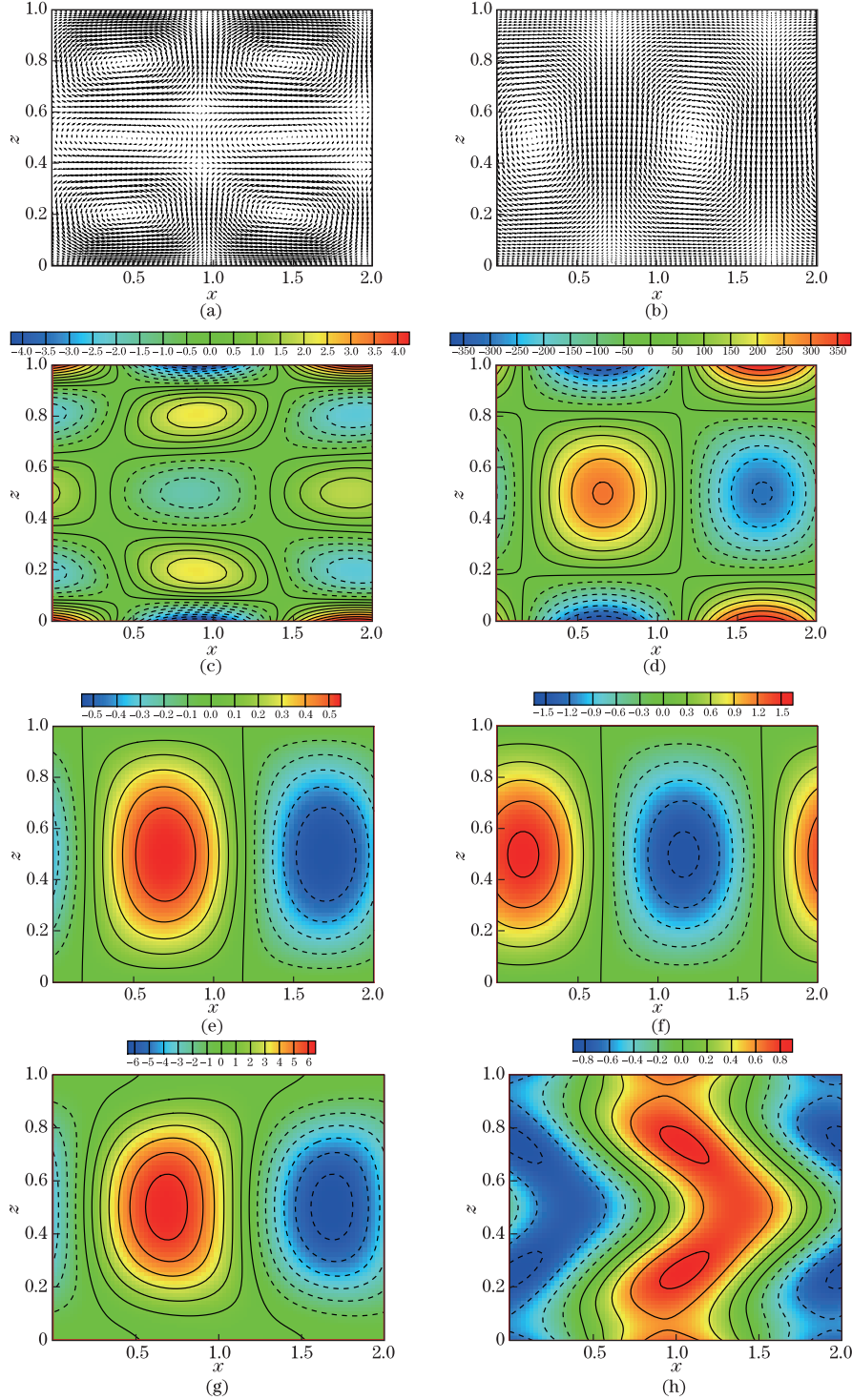


Fig. 7 Spatial patterns for initial optimal disturbance (left column) and maximum optimal amplification at $t_{\max} \approx 0.233$ (right columns) for velocity vector (u, w) (see (a) and (b)), spanwise vorticity ξ (see (c) and (d)), temperature θ (see (e) and (f)), and concentration c fields (see (g) and (h)), where $\alpha = 3.14$, $\beta = 0.0$, $\psi = -0.1$, $Ra = 1\,800$, $Re = 0.15$, $Pr = 10$, and $Le = 0.01$ ($N = 31$ least-stable spectra are used)

a three-layer cell vorticity structure, which is symmetrical about the centerline of the channel. After the transient growth, the three-layer cells are developed into one cell with a larger vorticity structure (see Fig. 7(b)). The strength of the velocity vector field are not plotted in Figs. 7(a) and 7(b). In order to clearly understand the large amplification from the optimal disturbance, the contour curves of the spanwise vorticity are exhibited in Figs. 7(c) and 7(d). The spanwise vorticity can be obtained by

$$\widehat{\xi} = \mathcal{D}\widehat{u} - i\alpha\widehat{w}.$$

It is clearly seen from these two subfigures that the spanwise vorticity achieves a large amplification with the order $O(10^2)$. Moreover, it is found that the largest spanwise vorticities occur near the upper and lower rigid walls.

Furthermore, for the temperature and concentration fields shown in Figs. 7(e), 7(f), 7(g), and 7(h), after the transient growth from the optimal disturbance, the amplitude of the temperature field magnifies three times and that of the concentration field decreases to one-eighth of the initial amplitude. It is also seen that the contour of the concentration field has a complex distort shape at the time of the maximum optimal amplification.

4 Conclusions

In this paper, a large transient growth with the order $O(10^2)$ is revealed for the Poiseuille-Rayleigh-Bénard flows of binary fluids with the Soret effect for negative separation factors due to the subcritical unstable characteristic. It is interesting that this large transient growth can be produced only by the two least-stable modes for small Reynolds numbers. Large Reynolds numbers even have an obvious stabilization effect on the transient growth for moderate wave numbers. Thus, the negative separation factor and the Rayleigh number play a key role for the large amplification of energy norm.

The spatial patterns of the optimal disturbances for the large transient growth are plotted for two-dimensional pure streamwise disturbances. For the velocity vector field, the initial three-layer cell vorticity structure is found and developed into one cell at the time t_{\max} when the maximum optimal amplification with the order $O(10^2)$ is obtained.

Finally, it should be noticed that, based on the thorough understanding of the linear transient mechanism, the work in this paper can be further extended to the study of the optimal control on the Poiseuille-Rayleigh-Bénard flows with the Soret effect. This will be our future research object.

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